



Dreaming
Collaborating
Innovating
Exploring
Trailblazing

Applications of Flow Control to a Commercial Aircraft In Memory of John Lin

Arvin Shmilovich¹, Paul Vijgen²

- ¹ Boeing Research and Technology
- ² Boeing Commercial Aircraft (Retired)

Advanced Modeling & Simulation (AMS) Seminar Series NASA Ames Research Center, May 25th, 2023

Producing Leading

Creating

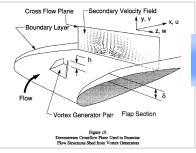
Researching

Analyzing

In Memory of John Lin 1957 - 2021



A prolific researcher at NASA Langley, and a great colleague and friend



Passive Flow Control with Micro Vortex Generators



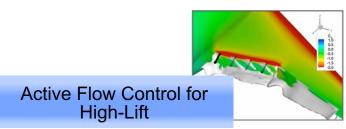


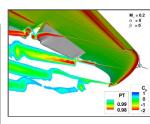
Full-Scale Active Flow Control Enhanced Vertical Tail

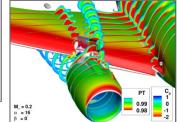




High-Lift Common Research Model





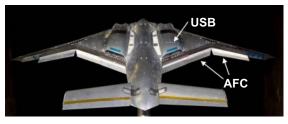


NASA/Boeing AFC Collaborations

- ATT (2002)
 - Prop STOL
 - With AFRL



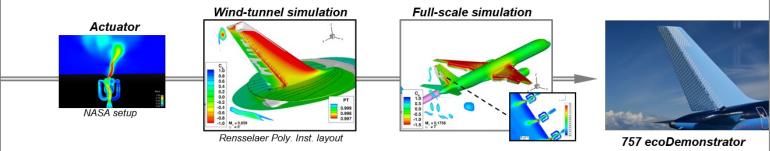
- AJACS (2012)
 - STOL USB/AFC
 - With AFRL



AIAA 2013-1097 AIAA 2013-2796

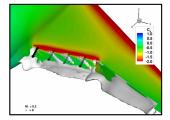
Boeing 757 ecoDemonstrator (2012-2015)

- Vertical tail



AIAA J, Vol. 56, No. 9, 2018 AIAA J, Vol. 56, No. 12, 2018

- CRM/AFC (2016)
 - Simple hinge flap





AIAA 2017-0321 AIAA 2017-0322

- Localized AFC (2020)
 - Small modification, high payoff

AFC Active Flow Control

ATT Advanced Theater Transport

AJACS Advanced Joint Air Combat System

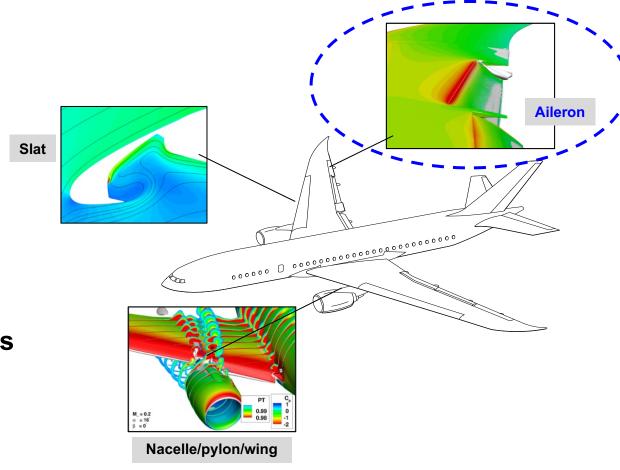
STOL Short Takeoff and Landing USB Upper Surface Blowing

CRM Common Research Model

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Motivation

- Improve airplane performance by increasing L/D, C_L, C_{L,max} during high-lift
 - Higher payload, longer range, shorter runway (<u>AIAA 1991-1527</u>)
 - $\Delta(L/D)$ = +1% in takeoff is equivalent to a 2,800lbs increase in payload or a 150nm increase in range
 - A 1.5% increase in C_{L,max} is equivalent to a 6,600lbs increase in payload for a fixed approach speed
- Localized AFC concepts
 - Aileron
 - Wing Leading Edge
 - Slat
 - Nacelle/pylon/wing
- NASA/Boeing collaboration
 - NASA PMs John Lin, Latunia Melton
 - Boeing PM Rene Woszidlo
- Study described in three SciTech 2023 papers
 - **1. Aileron** AIAA 2023-0655
 - 2. Wing LEs AIAA 2023-0656
 - 3. System Integration AIAA 2023-0657







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Flow Control for Enhanced Aileron Effectiveness on a Commercial Aircraft

Arvin Shmilovich¹, Yoram Yadlin¹, Paul Vijgen², Rene Woszidlo¹

¹ Boeing Research and Technology

² Boeing Commercial Aircraft (Retired)

AIAA SCITECH 2023 AIAA-2023-0655 Session: APA-24, Flow Control Applications Including Experiment and Computation IV Tuesday Jan 24, 2023

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Leading
Creating
Researching
Analyzing

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Numerical Procedure

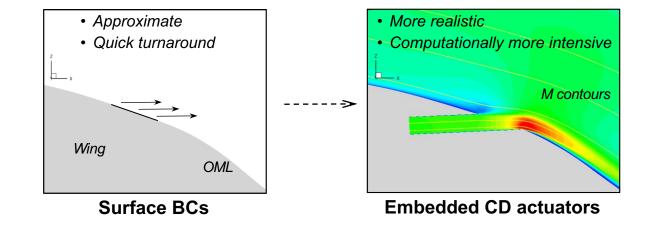
OVERFLOW

- Overset grid system
- Special boundary conditions for various actuation techniques introduced by Boeing¹⁻³
- Accuracy⁴
 - Upwind differencing, O(2)
 - Time-stepping scheme, O(2)
- Method validated for various AFC applications^{5,6}

AFC modeling

- Steady actuation (has practical advantages⁷)
 - Surface Boundary Conditions (BCs)
 - Convergent/divergent (CD) nozzle
 - · Discrete CD ducts

- 1 AIAA J., Vol. 49, No 3, 2011
- 2 AIAA 2016-3309
- 3 Notes on Num. Fluid Mech., Springer, Vol. 145, 2020
- 4 AIAA J., Vol. 54, No. 8, 2016
- 5 J. of Aircraft, Vol. 45, No. 5, 2008
- 6 AIAA J., Vol. 57, No 1, 2019
- 7 AIAA 2023-43101



CD = convergent/divergent

CFD Validation vs. NFAC Wind-Tunnel and Flight-Test – AFC-On

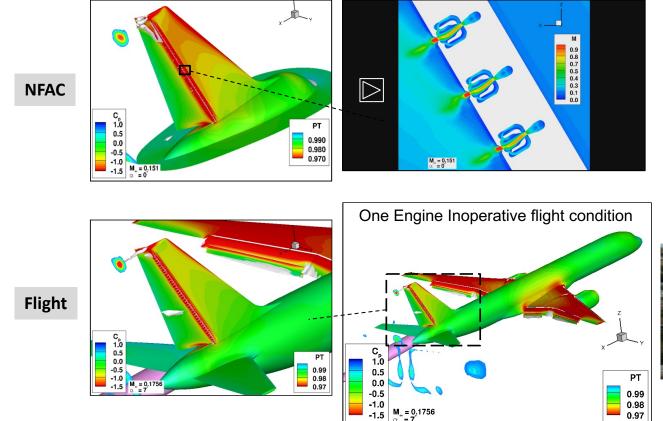
FOs

Experiment - FOs on the vertical tail

- NASA Ames NFAC
- Flight test Boeing 757 ecoDemonstrator¹

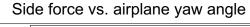
CFD - OVERFLOW²

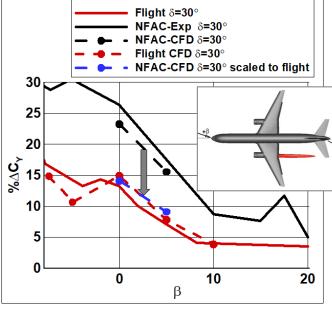
Unsteady actuation











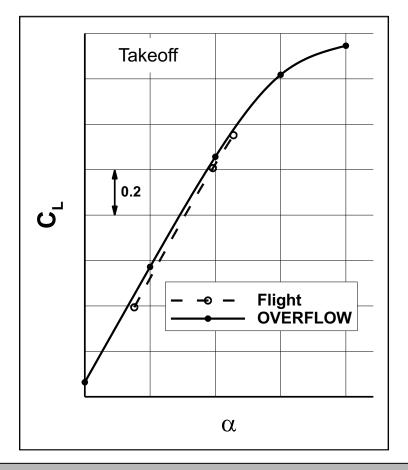
Acceptable agreement given the uncertainties in flight data

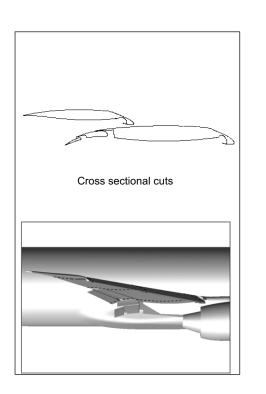
¹ AIAA J, Vol. 56, No. 9, 2018

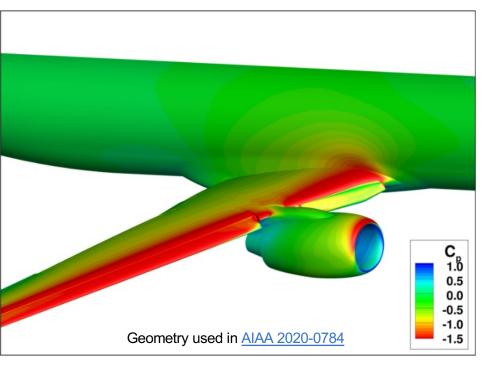
² AIAA J, Vol. 56, No. 12, 2018

CFD Validation vs. Flight Data – AFC-Off

- No experimental data is available for the AFC applications considered in this study
- Limited validation for a similar baseline configuration







Good agreement for high-lift configuration

Reference Aircraft and Grid Setup

Notional short/medium-range twin-engine airplane

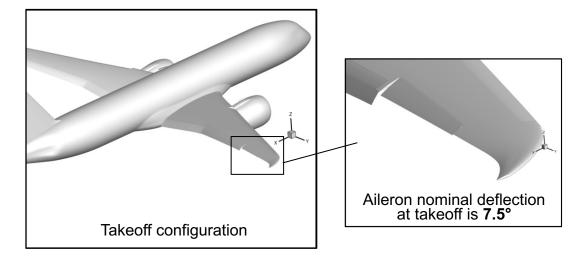
- Relevant to future platforms
- High-lift system Krueger/slats, single-slotted flap
- Takeoff flap setting

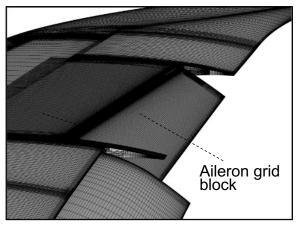
Objective – Higher aileron deflection + AFC

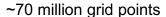
Increase L/D, C_L, C_{L,max}

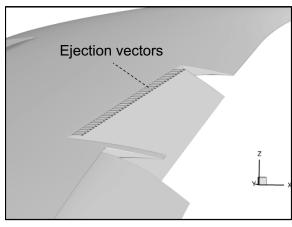
Initial CFD setup for AFC

- Aileron deflected to 25°
- AFC
 - Surface BCs (initially)
 - · Applied on a strip of constant width along the hinge line
 - Jet angle is specified
 - AFC intensity is determined by PR, TR
- Flow conditions
 - M=0.20
 - Re = 6.10^6
 - Fully turbulent (SA turbulence model)







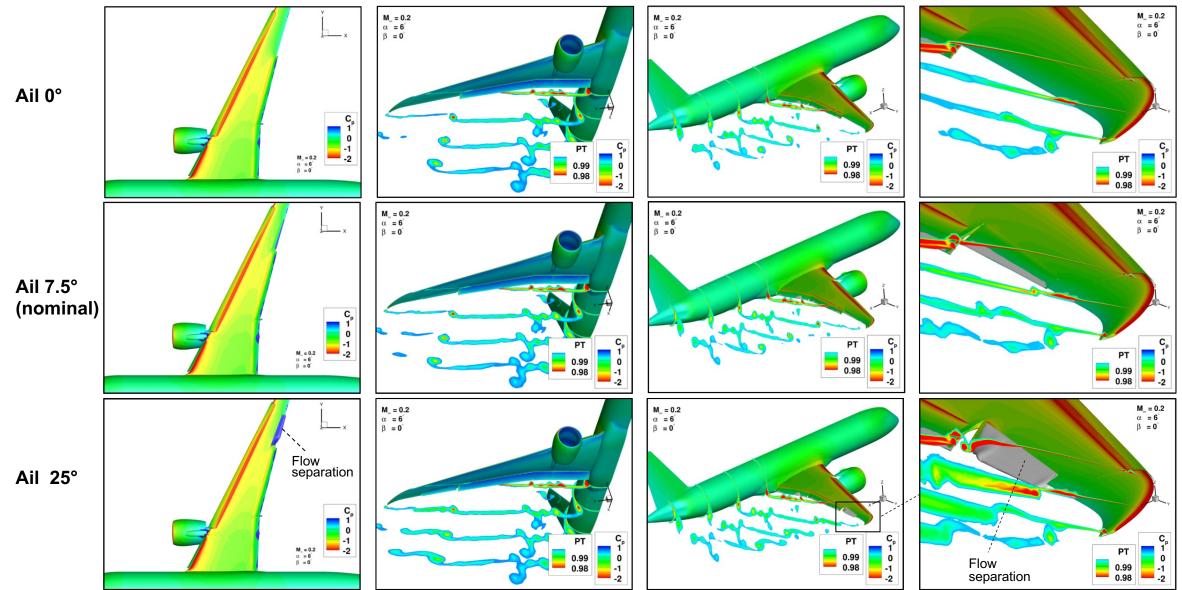


AFC applied at the hingeline

Aileron Deflections (Baseline, AFC Off)

Cp = Pressure coefficient on surfaces
PT = Normalized total pressure on wake cuts

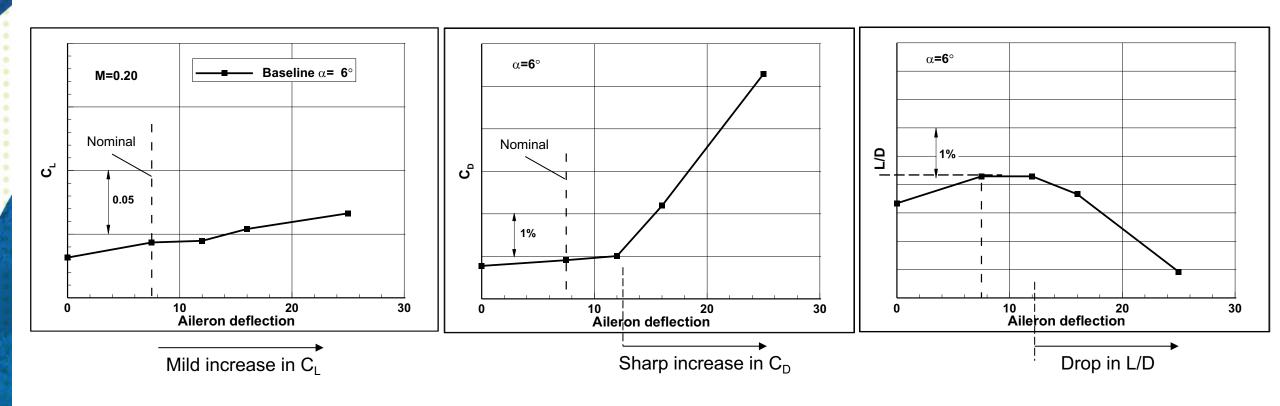
Nominal takeoff, $\alpha=6^{\circ}$



Aileron Deflections (Baseline, AFC off)

Motivation for AFC – augment L/D beyond the level achieved with the nominal deflection

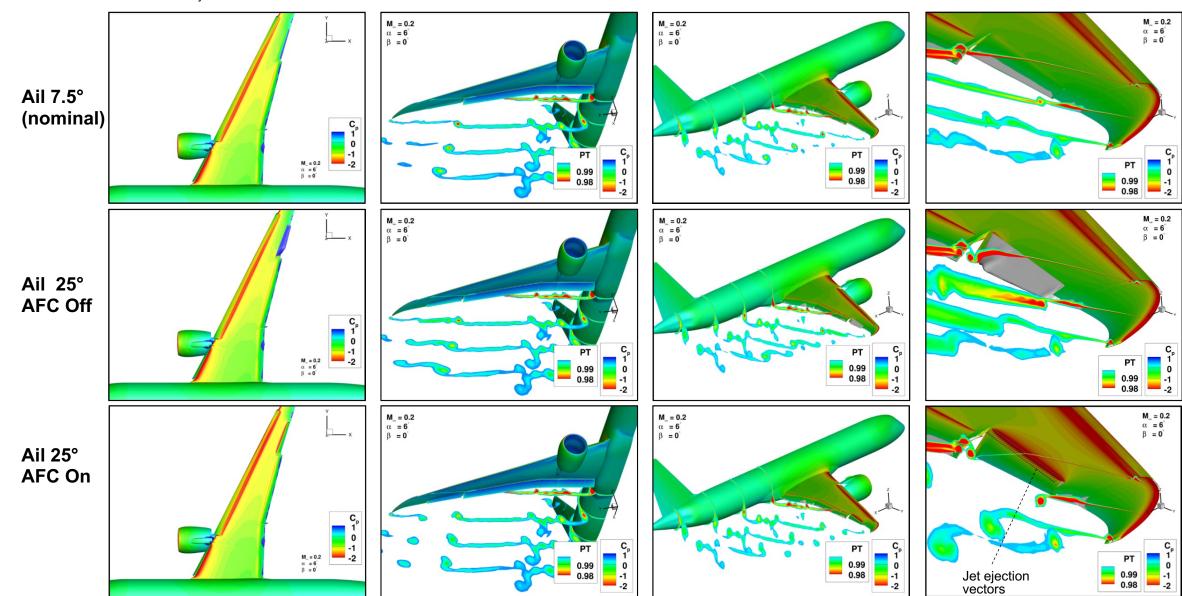
Aileron deflections 0°, 7.5°, 12°, 16°, 25°



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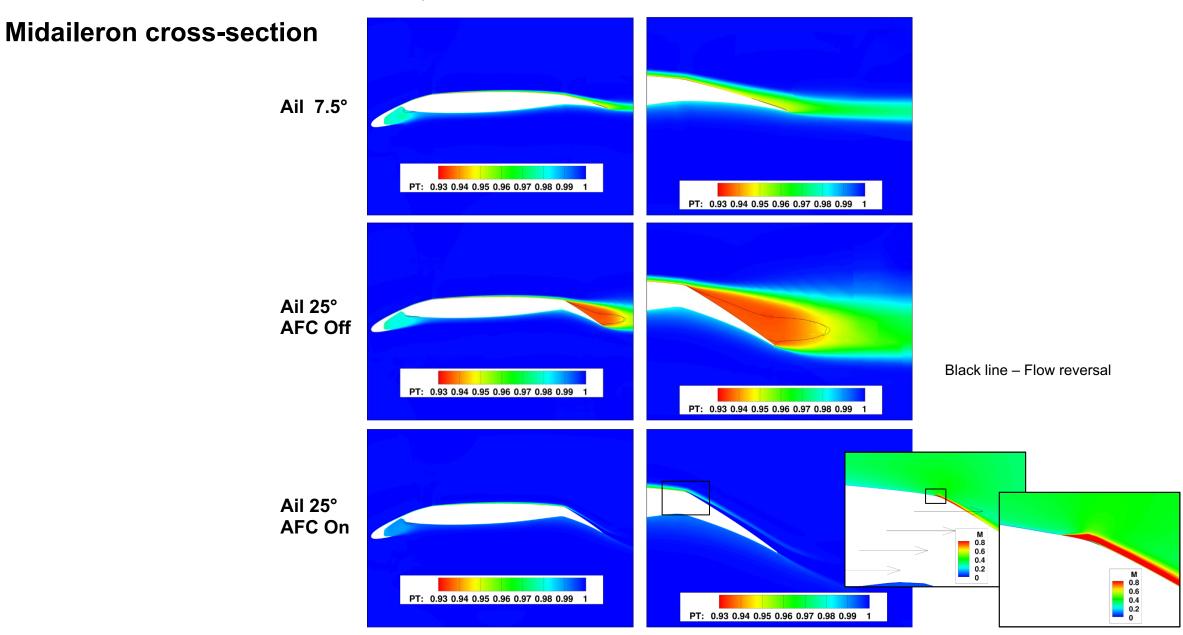
Effects of AFC – PR=2.0, Streamwise Jet

Surface BCs, Effective h_{jet}/c_{midaileron}≈0.008



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Effects of AFC – PR=2.0, Streamwise Jet

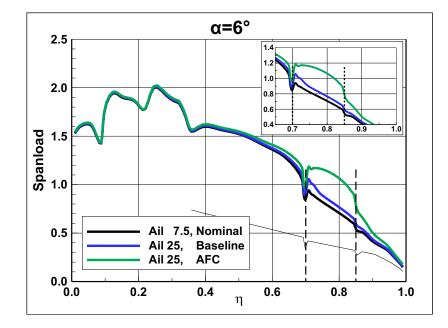


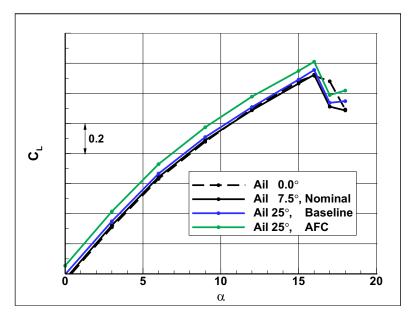
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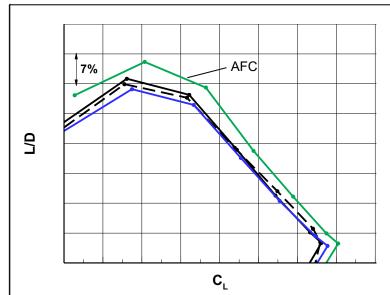
Effects of AFC – PR=2.0, Streamwise Jet

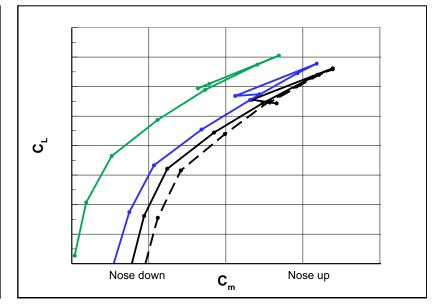
AFC impact on aero performance + integration

- Increased C_L over the practical lift range, including C_{L,max}
- + Reduced flow separation + closer to elliptical spanload results in reduced drag
- + Hence significant increase in L/D is predicted
- Aft loading results in increased nose-down pitching moment, resulting in potential trim drag penalty
- Higher wing bending moments
- Aeroelastic effects (negative twist)





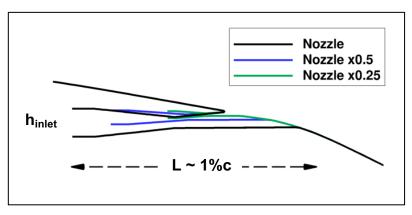




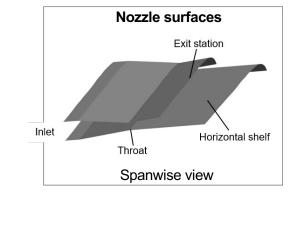
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Convergent/Divergent (CD) Nozzle

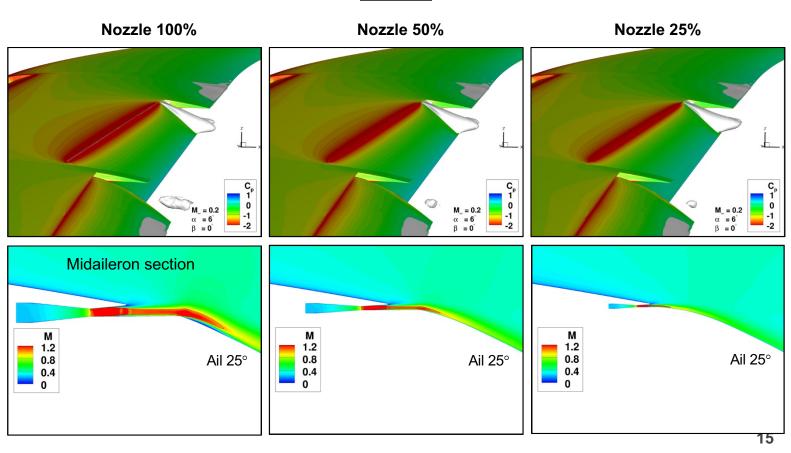
- Realistic implementation of AFC
 - CD in the vertical plane
 - 2D nozzle cross-section identical along the span, edge-to-edge
 - Mild angle of the divergent section to prevent separation
- Grid ~85 million
- Nozzle operates at low PR
 - Nozzle area is large



h_{inlet} /L ≈ 0.11 c = local wing chord



PR=2.0

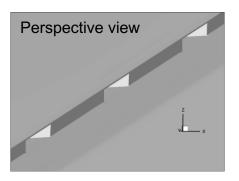


Discrete Convergent/Divergent Ducts

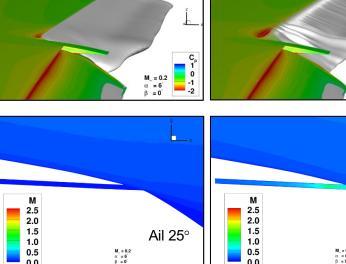
- Derived from the NASA Fluidic Oscillators
 - Are used in DARPA/CRANE X-65 AIAA 2023-2310, AIAA 2023-43101
- Convergent/divergent in wing planform
- Grid ~186 million
- Ducts are very efficient (reduced mass flow), but require high PR

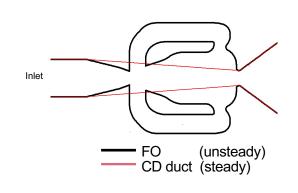
Baseline (PR=1)

- 78 ducts
- Total duct area is very small

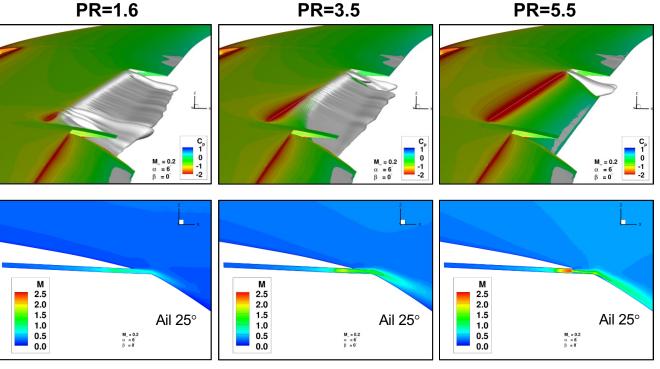








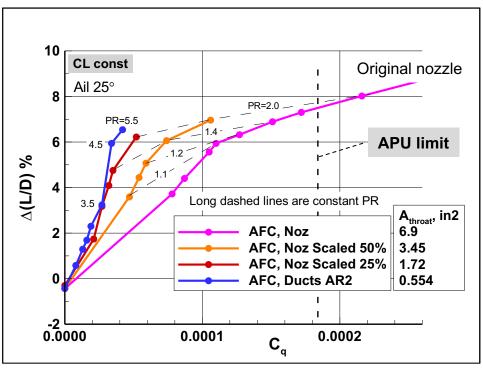
FO = Fluidic Oscillator



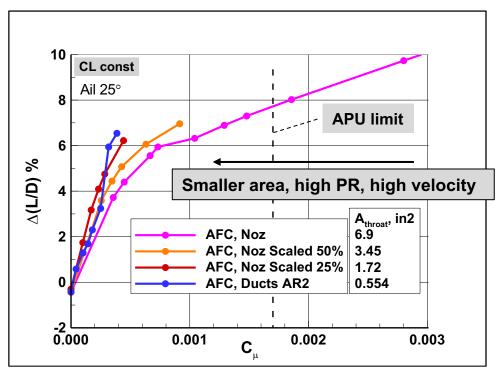
¹ Shmilovich, Khodadoust, Colletti, Ansell, 'Steady versus Unsteady Pneumatic Flow Control and Aspects of Practical Integration'

Assessment of AFC Layouts – Nozzles vs Discrete Ducts

- Both nozzles and discrete ducts are potential candidates
- Better performance is achieved with smaller area, but requires higher PR
- The available air source (PR, C_q, etc.) will drive the selection of nozzle type/size



Mass flow coefficient

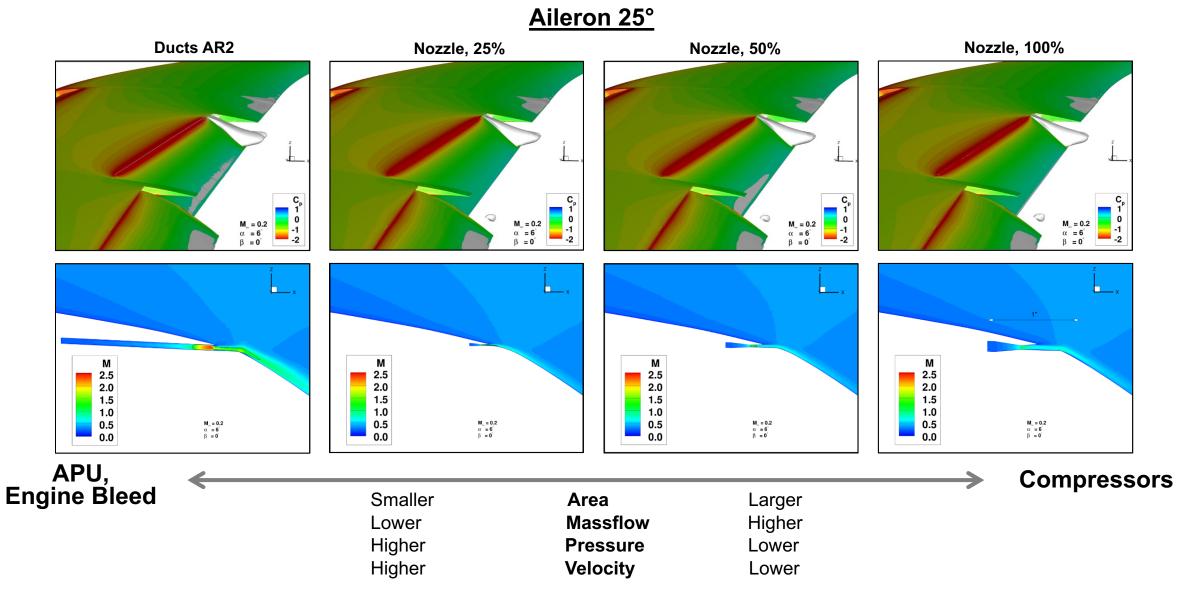


Momentum coefficient

△L/D~6% achievable with onboard supply

Aspects of Integration

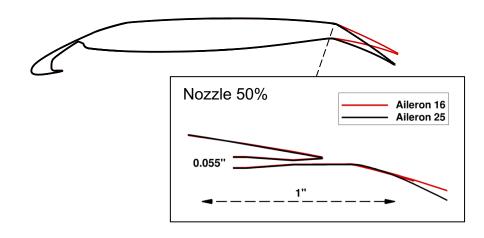
Actuation types will be paired up with potential sources

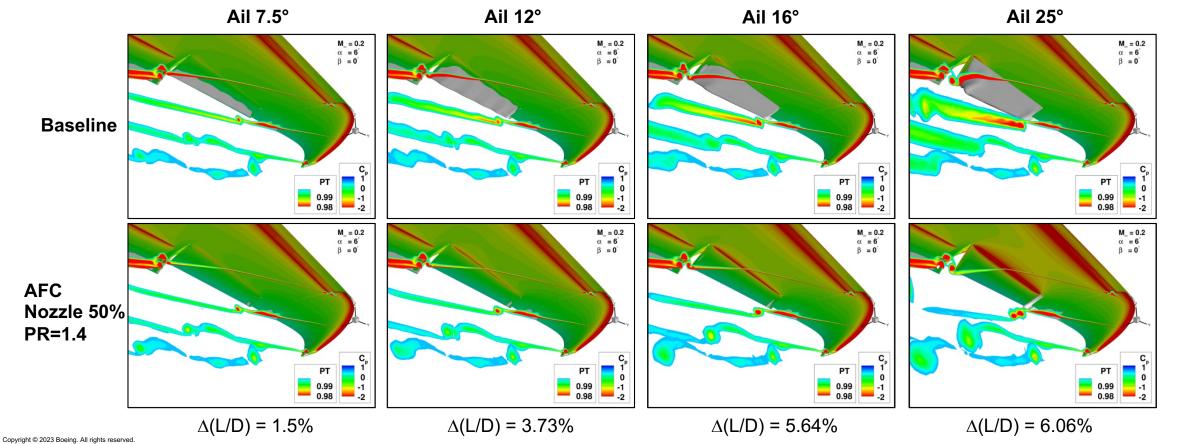


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More Practical Aileron Deflections

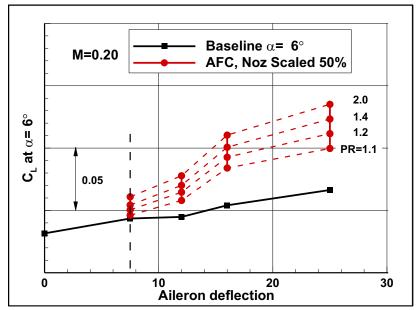
- Consider lower deflections (25° was used up to this point)
 - More acceptable hinge moments for aileron actuators
 - Lower wing bending moments
 - Lower trim drag

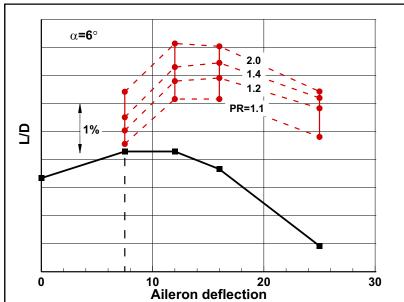


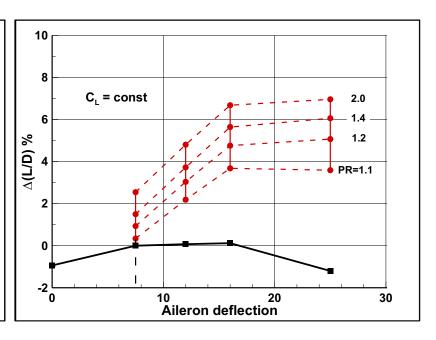


Effects of Aileron Deflections (Nozzle 50%)

- The best aero performance is in the range of 16°-25° (takeoff flap setting)
 - Proportionately smaller gains at 12° and 7.5°
- Selection of aileron deflection will likely be influenced by integration factors





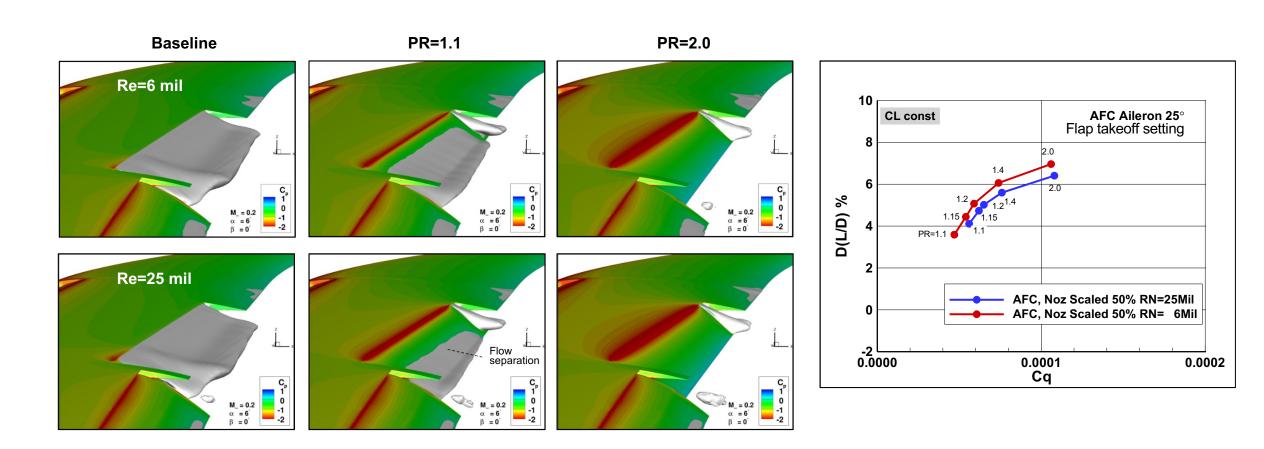


Maximum L/D gain is achievable with aileron 16°

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Reynolds Number Effects

Lower viscous effects at high RN results in slightly reduced AFC effects

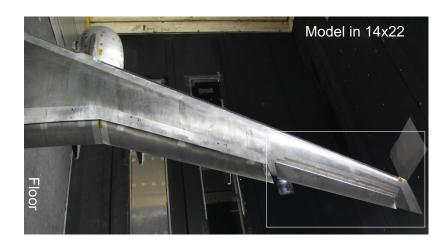


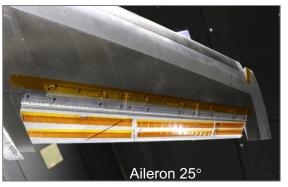
M_∞=0.20 α=6°

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Conclusions – Aileron at Takeoff

- Both elongated CD-nozzles and discrete CD-ducts are promising candidates
- Gains in L/D ~6% and C_{L,max} ~2.5% can be achieved with onboard sources
- Significant gains are obtained at smaller aileron deflections
 - Ease of integration
- Flight Reynolds number indicates slightly reduced AFC effects
- Landing results in similar AFC effects
- Experimental confirmation of the AFC approach is currently underway
 - CRM-HL tested at the NASA LaRC 14x22 tunnel (Feb.-March 2023)





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Applications of Flow Control to Wing High-Lift Leading Edge Devices on a Commercial Aircraft

Arvin Shmilovich¹, Yoram Yadlin¹, Paul Vijgen², Rene Woszidlo¹

¹ Boeing Research and Technology

² Boeing Commercial Aircraft (Retired)

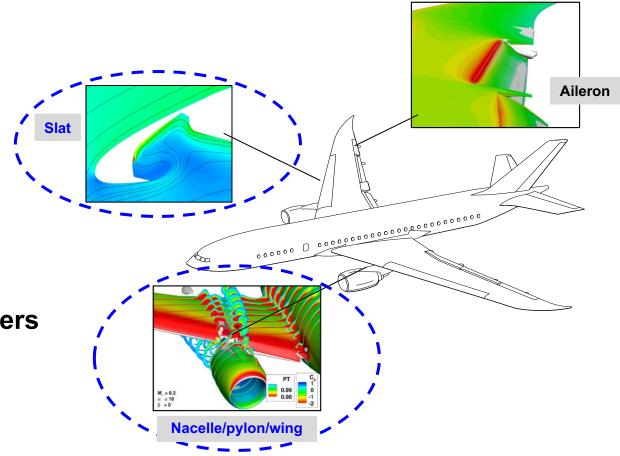
AIAA SCITECH 2023 AIAA-2023-0656 Session: APA-24, Flow Control Applications Including Experiment and Computation IV Tuesday Jan 24, 2023

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Analyzing

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Motivation

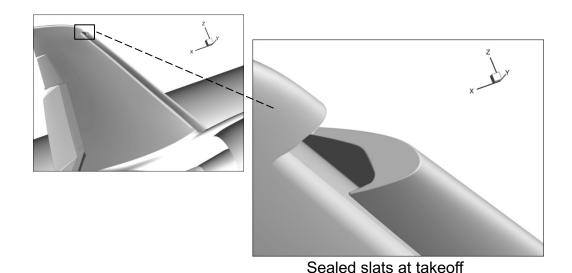
- Improve airplane performance by increasing L/D, C_L, C_{L,max} during high-lift
 - Higher payload, longer range, shorter runway (AIAA 1991-1527)
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- Localized AFC concepts
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 - 3. System Integration AIAA 2023-0657

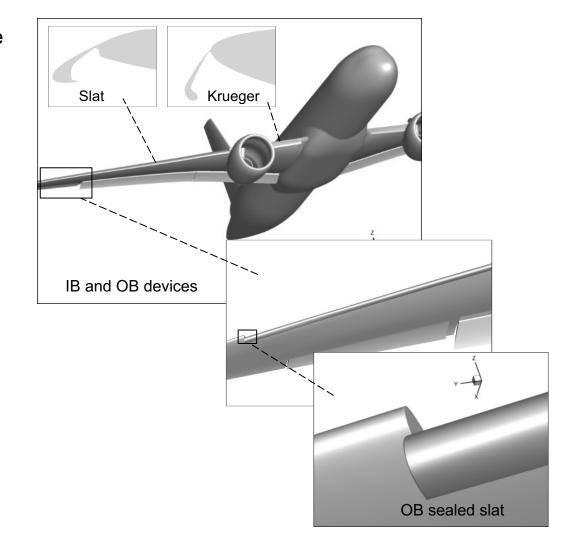


Reference Aircraft

Notional short/medium-range twin engine airplane

- High-lift system Krueger/slats, single-slotted flap, nacelle chine
- Takeoff flap setting



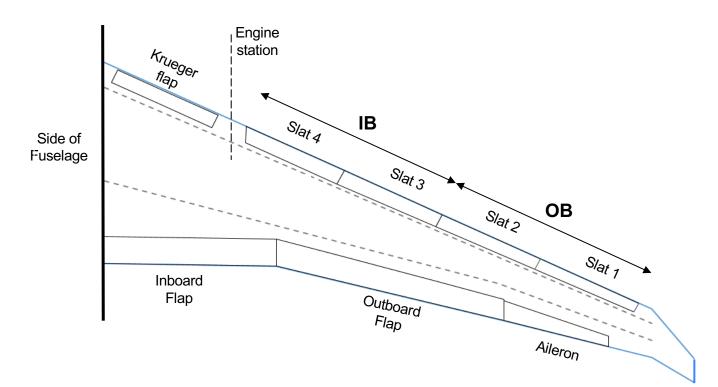


OB = outboard IB = inboard

25

Potential Fluidic Sources

- Proximity to potential fluidic sources are an important factor for the design of an AFC system
- Potential sources at the engine strut
 - Engine bleed
 - APU
 - Wing anti-ice system (WAI)
 - Selected slats are equipped with WAI, which is a source of hot air (high T helps reduce mdot)
 - Local compressors



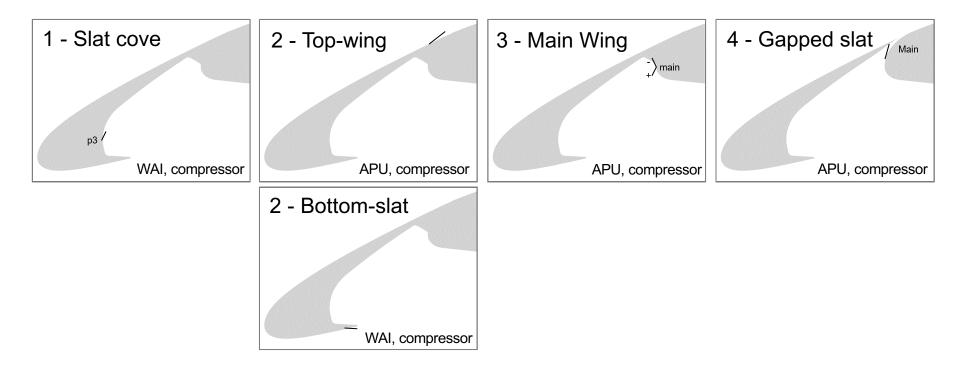
APU = Auxiliary Power Unit WAI = Wing Anti-Ice

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AFC at the Slats

Targeted Slat Applications

- Leverage the experience from <u>AIAA 2020-0784</u>
- Several AFC layouts have been considered



- Layouts 1 and 4 will be described here
- AFC with surface BCs

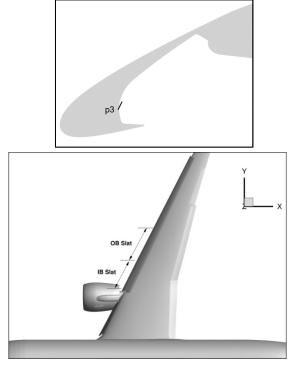
APU = Auxiliary Power Unit WAI = Wing Anti-Ice

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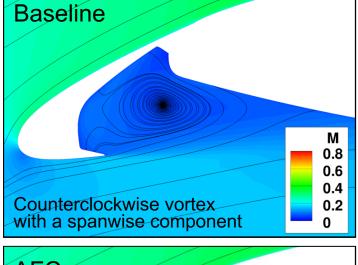
1 - Slat Cove

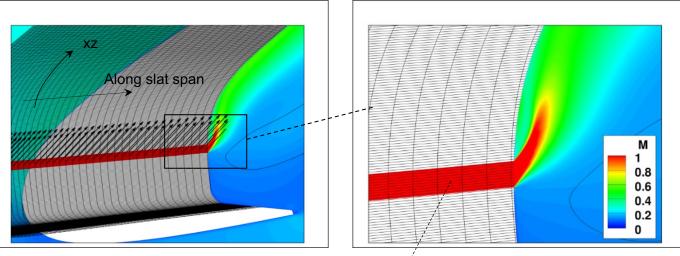
Numerical setup

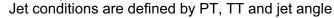
- Fine mesh ~100 million points
- Surface BC
- Jet efflux is at 20° off the local surface tangent in the upward direction

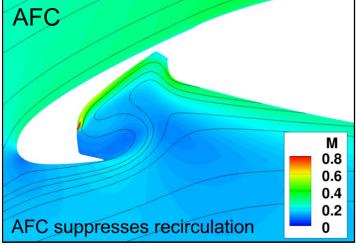


Slats 3 and 4









Every other 4 grid lines are shown in the xz direction

M contours are shown on a vertical streamwise cut at the mid OB slat

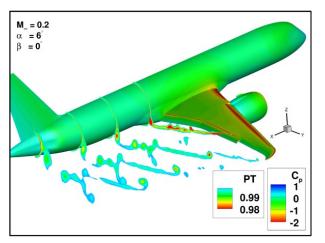
1 - Slat Cove

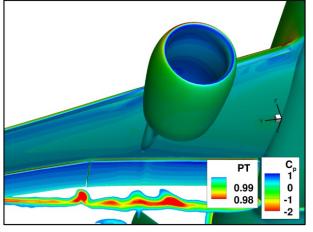
Cp = on surfaces

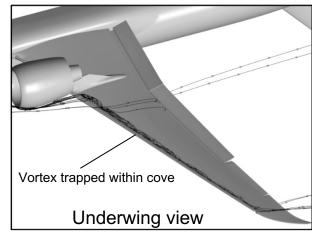
PT = Normalized total pressure on cuts

Baseline

- Flow is predominantly 3D in the vicinity of the slat
- Vortical flow forms in the slat cove and it emerges into the ambient flow towards the wing tip

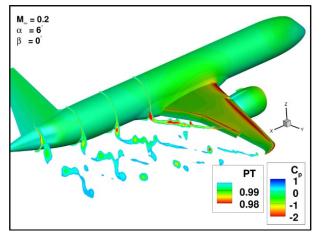


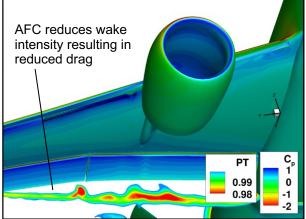


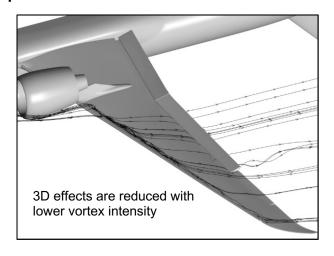


AFC

- Helps break the original counterclockwise flow, and helps curb spanwise flow and reduce 3D effects



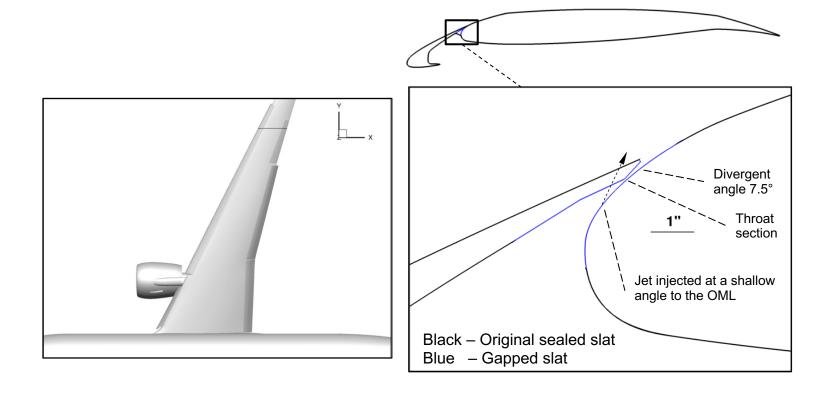




4 - Gapped Slat

Geometry setup

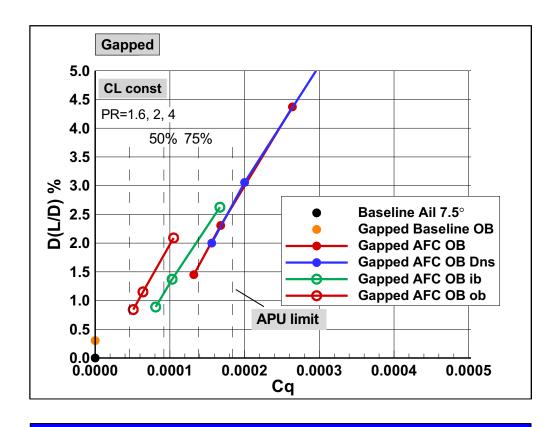
- Slat held at the same detent as in the sealed position
 - Preserves the general aero characteristics of the original wing
- Slat lower surface is modified to incorporate a convergent/divergent section



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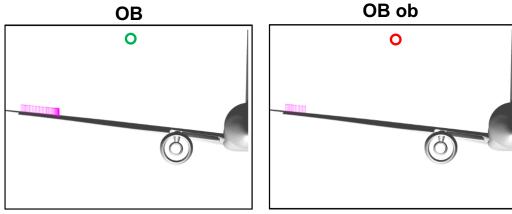
4 - Gapped Slat

Various AFC layouts land in the range of practical supply

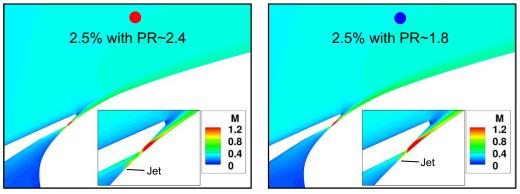


∆L/D up to ~2.5% achievable with onboard supply

Potential solution for wing-tip separation at high-α



Outboard actuation 'OB ob' is more effective



Downstream actuation is more effective

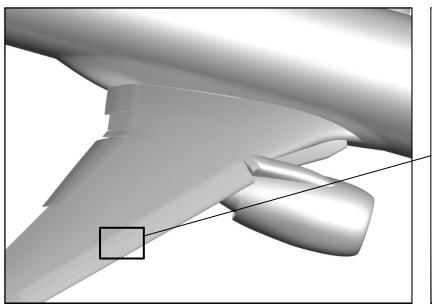
32

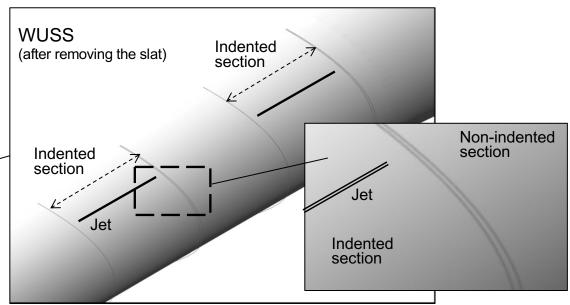
4 - Gapped Slat

Alternative implementation

- Wing can be modified
 - Designed to produce a convergent section

Potential mitigation of high-α wing tip separation





When the slat is in the sealed position

- Indented sections become gapped
- Non-indented sections remain fully sealed

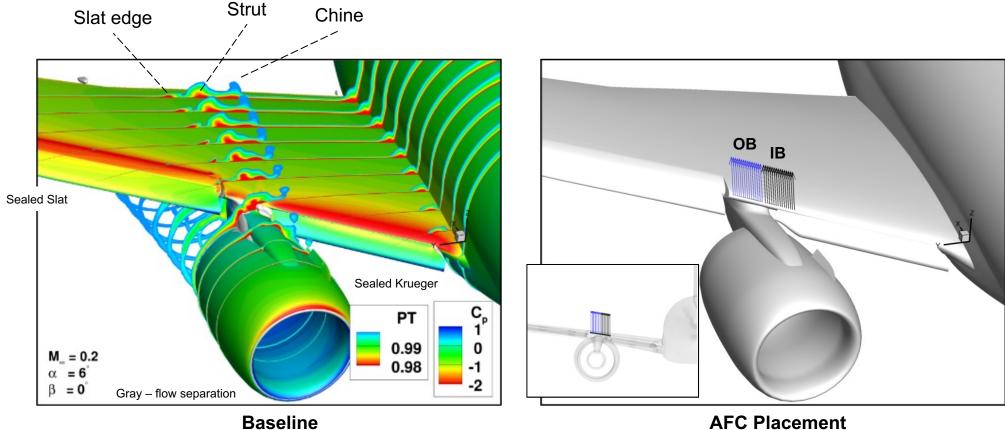
WUSS = Wing Under Slat Surface

AFC at Nacelle/Pylon/Wing

Nacelle/Pylon/Wing

Objectives

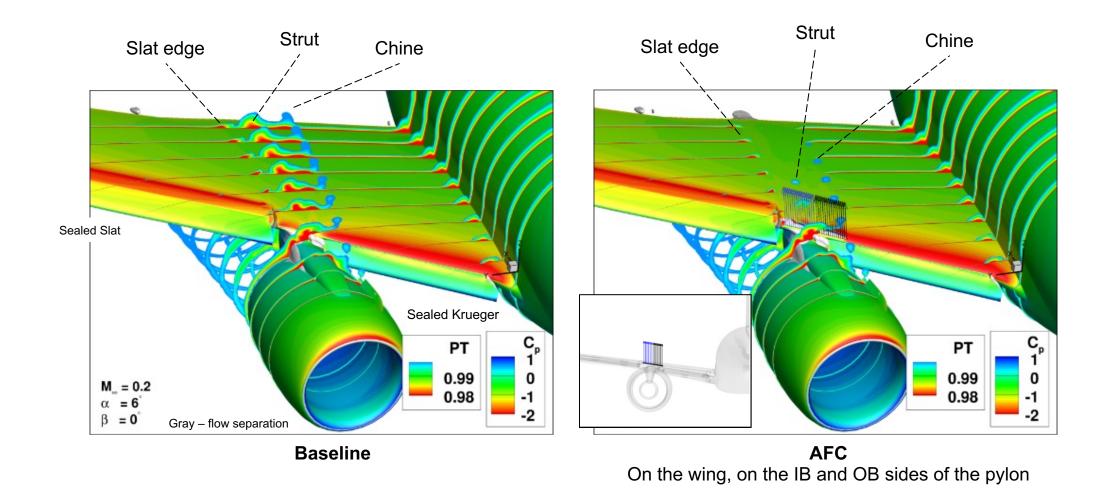
- Reduce wing/nacelle interference effects
- Potentially enabling better integration with the high-lift system at the pylon-engine
 - Especially important for integration of UHBR engines in future airplanes (reduced weight, maintenance)



On the fixed wing LE on both sides of the pylon station

Nacelle/Pylon/Wing at α =6°

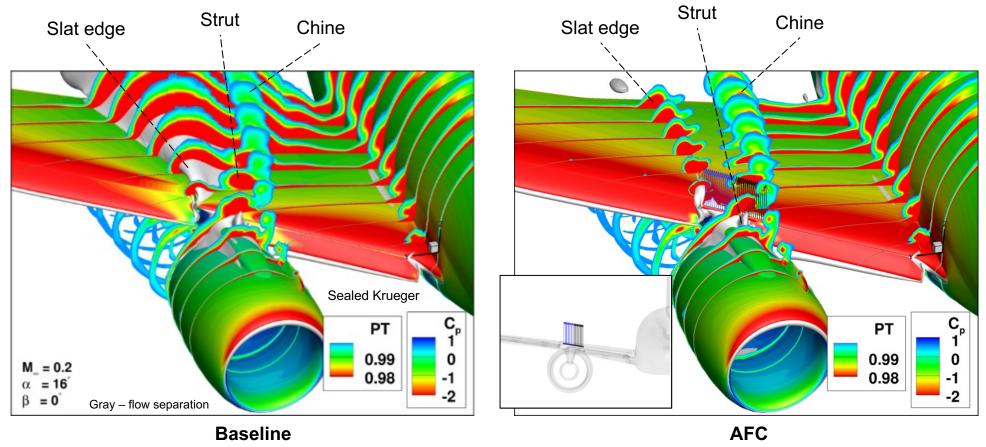
Intensity of vortex elements and wake is substantially reduced by actuation



36

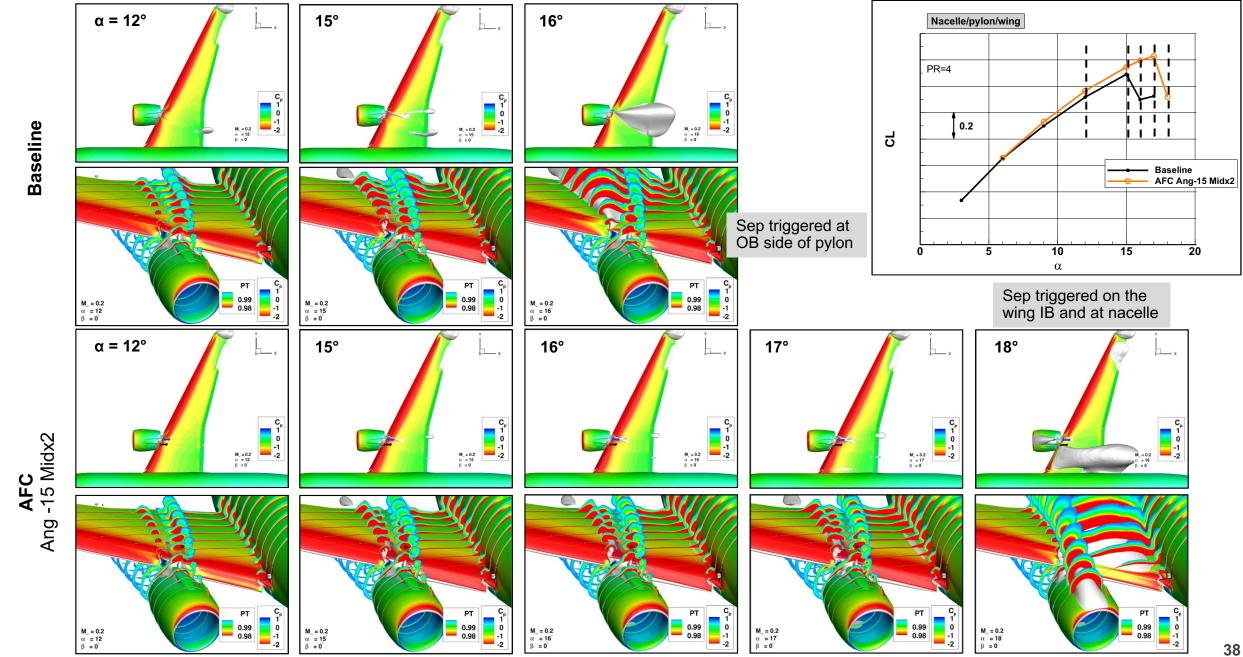
Nacelle/Pylon/Wing at α=16°

AFC helps reduce separation from slat edge and strut



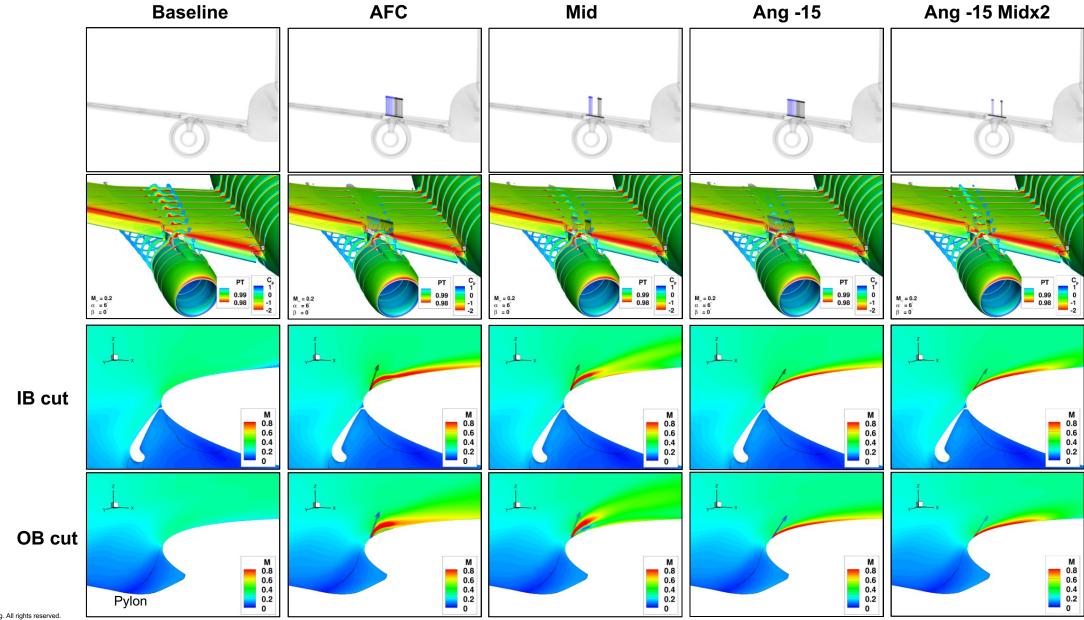
On the wing on the IB and OB sides of the pylon

Nacelle/Pylon/Wing – α Sweep



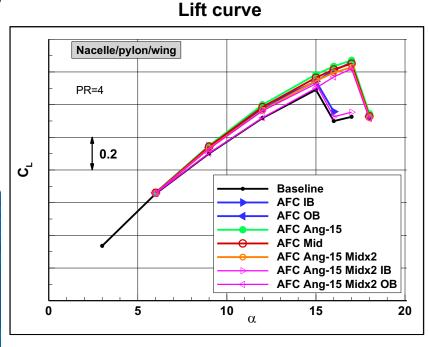
Nacelle/Pylon/Wing – AFC Patterns (α=6°)

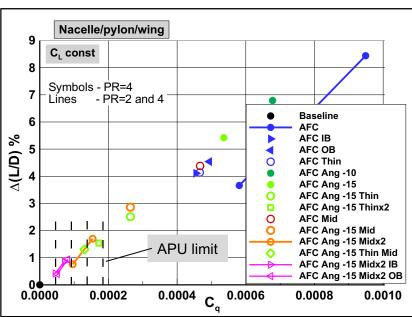
Jet size and orientation



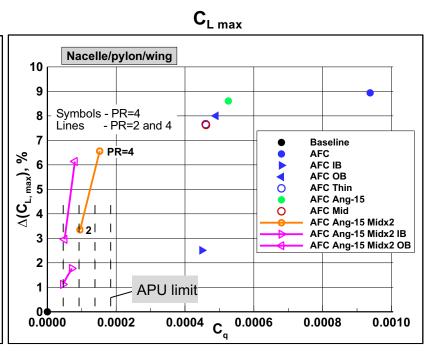
Nacelle/Pylon/Wing – AFC Patterns

Shallow jet angle is effective OB actuation much more effective (takeoff setting)





L/D at nominal takeoff

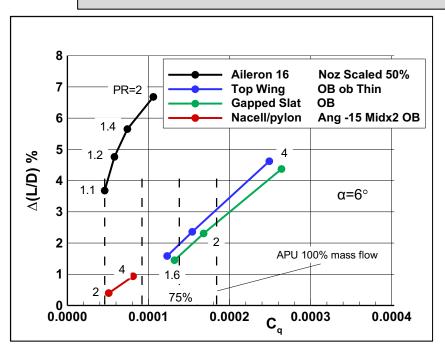


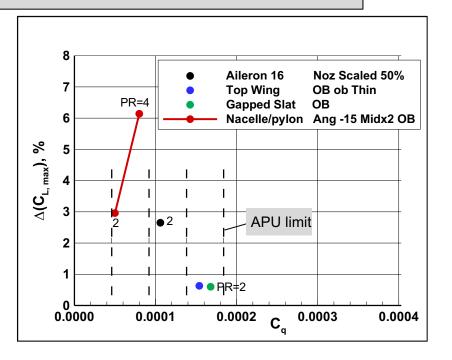
ΔL/D ≈ 1-1.5% ΔC_{L,max} ≈ 6% Baseline includes nacelle chine

Conclusions – Aileron & Wing LE

• Takeoff gains in CFD-predicted L/D of up to \sim 6% and C_{L,max} up to \sim 6% can be achieved with onboard sources, depending on the application (aileron or LE)

Summary of AFC opportunities for the Aileron-16° and LE applications





System integration study conducted to identify promising candidates





Dreaming
Collaborating
Innovating
Exploring
Trailblazing

Conceptual Integration Studies of Localized Active Flow Control on the Wing of a Commercial Aircraft

Paul Vijgen¹, Alex Ziebart², Arvin Shmilovich³, Rene Woszidlo³

- ¹Boeing Commercial Aircraft (Retired)
- ² Boeing Commercial Aircraft
- ³ Boeing Research and Technology

SCITECH2023 AIAA-2023-0657 Session: APA-24, Flow Control Applications Including Experiment and Computation IV Tuesday Jan 24, 2023

Producing
Leading
Creating
Researching
Analyzing

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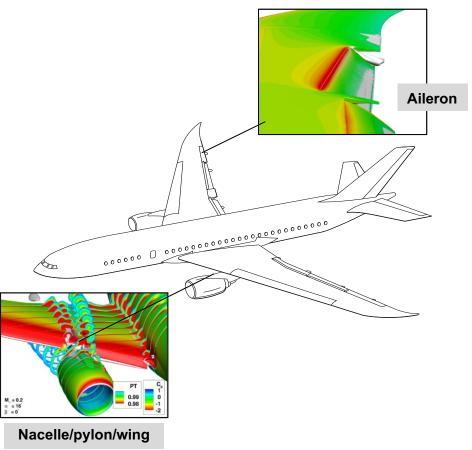
Conceptual Integration Study

Motivation

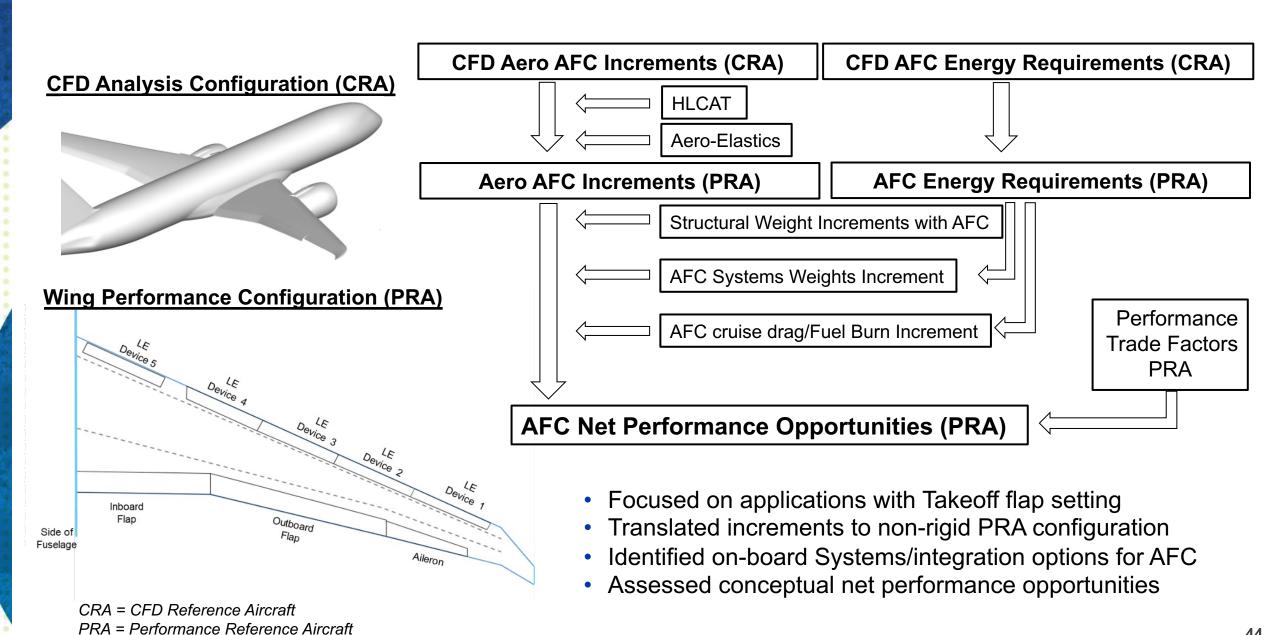
 Conduct airplane level Systems integration studies to assess potentially promising wing local AFC applications

Key steps

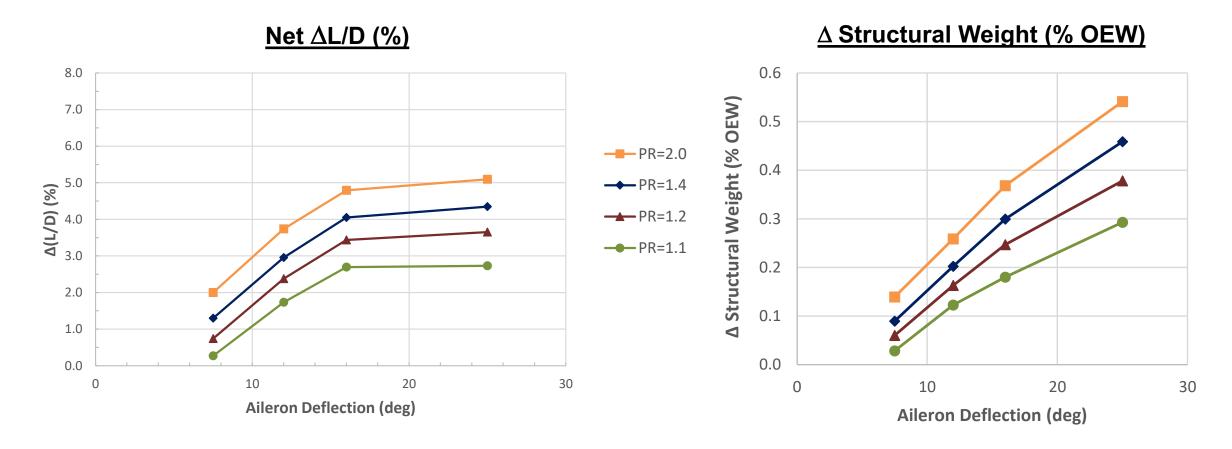
- AFC net aerodynamic benefits and structural penalties
- AFC energy sources, Systems layout and weight
- Estimated AFC net performance opportunities
- Summary and next steps



Configurations and Analysis Process

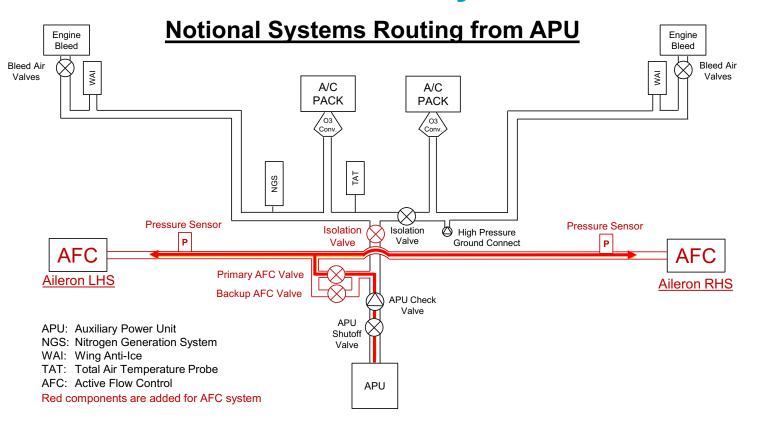


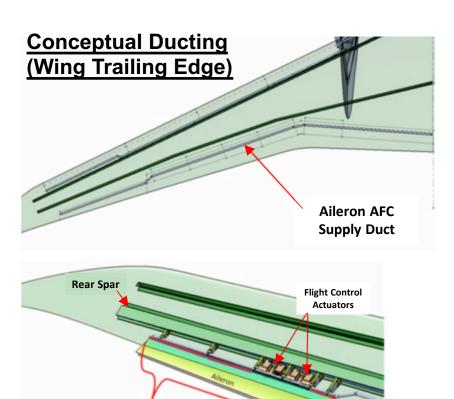
Aileron – Aerodynamic and Structural Increments (Takeoff)



- L/D increments adjusted for CRA-to-PRA geometry and for PRA aero-elastic, trim, and thrust effects
- PRA wing structural weight penalty 0.2 0.4% OEW (due to increased outboard loading)
- PRA net L/D improvement 3 5% with aileron deflections of 12° 16°

Aileron – APU Powered Systems





Approximate location of

Aileron AFC Actuators

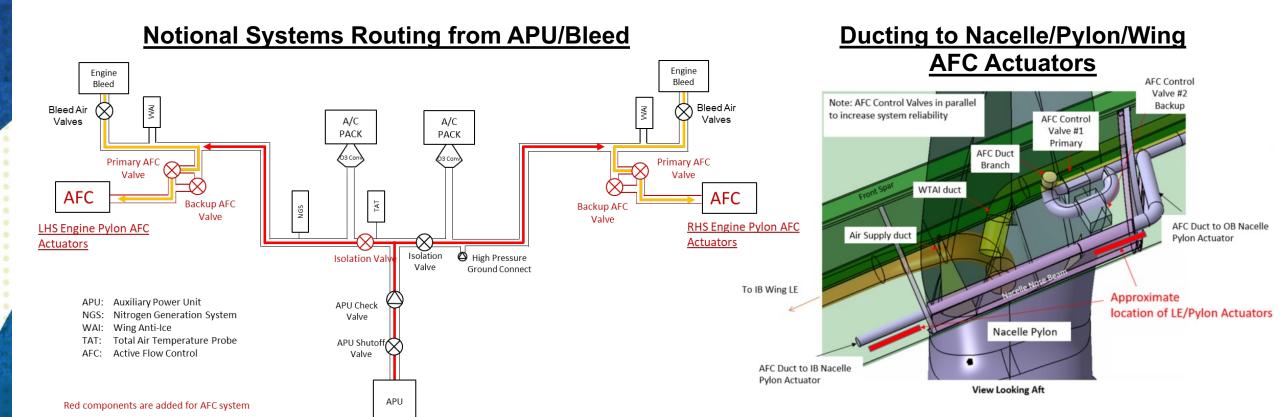
- APU load compressor can likely supply AFC energy (mdot and PR)
- Operation of APU during low-speed flight affects APU cost and maintenance
- Utilize existing ducting from APU to fuselage A/C Packs
- APU availability/reliability appears adequate further study needed (detailed FHA)
- Integrating AFC duct in wing trailing edge is possible (but challenging for smaller aircraft)
- AFC Systems' weight increments included in performance study

A/C = Air Conditioning FHA = Fault Hazard Analysis

AFC Duct

to Aileron

Nacelle/Pylon/Wing – APU/Bleed Powered Systems



- APU and engine bleed share common duct (minimal additional ducting and weight)
- APU is primary AFC flow source in Takeoff; engine bleed is primary AFC source in Landing
 - APU provides backup AFC source to engine bleed (and vice versa)
- Systems availability/reliability appears adequate further study needed (detailed FHA)
 - Balancing bleed demands for all pneumatic systems (WAI, EAI, A/C Packs, AFC)

FHA = Fault Hazard Analysis

WAI = Wing Anti-Ice System

EAI = Engine Anti-Ice System

Assessing Aircraft Performance Opportunities

Two Performance Scenarios Studied

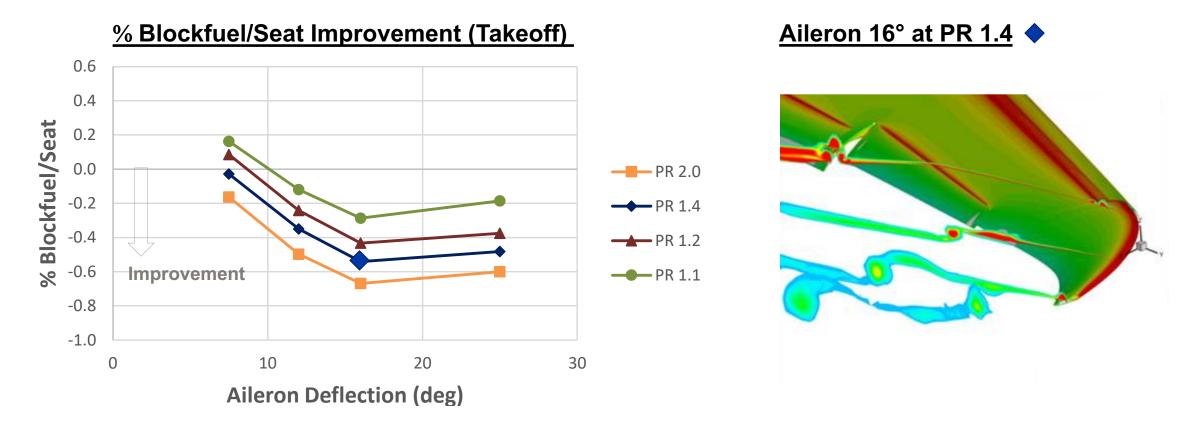
1. AFC affects Aircraft Sizing

- Wing Area, Engine Thrust, OEW, flap area, fuselage Takeoff attitude (incl. family stretch strategy)
- In Takeoff: L/D critical for Hi-Hot Takeoff sizing constraint → Fuelburn/seat opportunity
- In Landing: $C_{L,max}/C_{L,app}$ critical for V_{app} → Affects wing size/flap size → Fuelburn/seat opportunity

2. AFC does not affect Aircraft Sizing

- AFC can benefit airline operations (life-cycle airline value) to mitigate Hi-Hot Takeoff constraints
- Hi-Hot Takeoff payload increase and Engine Derate → airline operating cost opportunity

Sizing Scenario / Net Airplane Benefit - Aileron



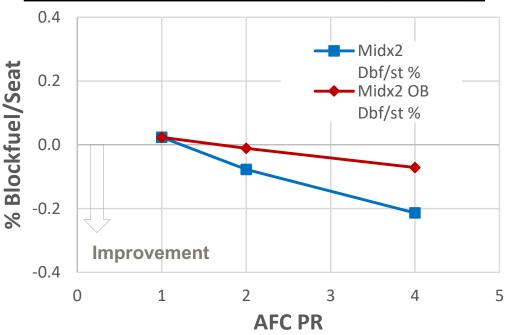
- Takeoff L/D is a key parameter that can affect sizing of wing area and engine thrust (Hi-Hot Takeoff)
- AFC related structural and Systems weight increments, and APU inlet & AFC actuator drag, are included
- APU-powered AFC could provide net **0.4 0.6**% blockfuel/seat improvement (relative to non-AFC baseline)

PR = AFC Actuator Pressure Ratio

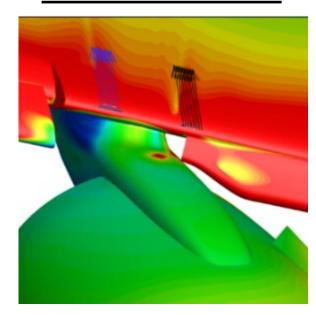
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Sizing Scenario / Net Airplane Benefit – Nacelle/Pylon/Wing





Midx2 AFC Actuation



- AFC concept studied provides L/D benefit in Takeoff (with PR 2 4)
- AFC related Structural and Systems weight increments, and APU inlet & AFC actuator drag, are included
- APU-powered AFC could provide net 0.1 0.2% blockfuel/seat improvement (relative to non-AFC baseline)
- Study did not address nacelle/pylon/wing AFC in Landing potentially larger benefits (impact on C_{Lmax})

Assessing Aircraft Performance Opportunities

Two Performance Scenarios Studied

1. AFC affects Aircraft Sizing

- Wing Area, Engine Thrust, OEW, flap area, fuselage Takeoff attitude (incl. family stretch strategy)
- In Takeoff: L/D critical for Hi-Hot Takeoff sizing constraint → Fuelburn/seat opportunity
- In Landing: $C_{L,max}/C_{L,app}$ critical for V_{app} → Affects wing size/flap size → Fuelburn/seat opportunity

2. AFC does not affect Aircraft Sizing

- AFC can benefit airline operations (life-cycle airline value) to mitigate Hi-Hot Takeoff constraints
- Hi-Hot Takeoff payload increase and Engine Derate → airline operating cost opportunity

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Non-Sizing Performance Scenario - Aileron

AFC Operational Opportunities

- More passengers (payload) for gradient-limited Hi-Hot Takeoffs
- Reduced engine thrust setting (derating) for non-gradient-limited Takeoffs

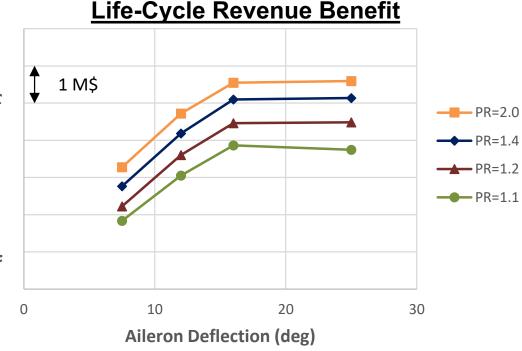
Life-Cycle Analysis with Takeoff L/D Increase

- AFC Systems, wing structural weight penalty and APU operations translate into fuel burn increase
- L/D increase offers potential net 5 8% increase in payload for gradient-limited Takeoffs
- Assumed 25% of Takeoffs are gradient limited; non-gradient limited Takeoffs benefit from engine derating
- Estimate net Life-Cycle Revenue Benefit is several \$M's per aircraft

AFC Operational Opportunities

Aileron droop (deg)	Net payload increase (gradient limited airports)	Block fuel change (economical mission)	Engine takeoff thrust derate (nongradient limited airports)
7.5	1.9%	+ 0.12%	0.8%
12	5.6%	+ 0.18%	2.0%
16	8.0%	+ 0.23%	2.9%
25	8.3%	+ 0.32%	3.1%





Summary and Next Steps

Summary

- CFD was used to explore AFC opportunities and requirements
- Conceptual study indicates wing AFC integration is feasible with relevant aircraft net performance benefits
- Study resources mostly focused on aileron AFC, but found encouraging results for LE application

Next steps

- Validation of CFD results
 - CRM-HL with aileron AFC tested at NASA-LaRC 14x22-ft tunnel (Feb-March 2023)
- Further studies on wing AFC integration and performance opportunities
 - FHA for studied AFC energy sources (APU, Bleed, other)
 - Detailed performance/sizing for Takeoff and Landing scenarios
 - Further CFD and integration definition of LE applications (UHBR nacelle junction and slat/wing tip)
 - Detailed Systems design and validation of integrated AFC hardware (ground and flight testing)

LE = Leading Edge FHA = Fault Hazard Analysis UHBR = Ultra High Bypass Ratio

References

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- Woszidlo, R., Shmilovich, A., and Vijgen, P., "Low-Speed Performance Enhancement using Localized Active Flow Control – Program **Overview** and Summary", *NASA Technical Reports Server*, April, 2022, document ID: <u>20220006728</u>.
- Shmilovich, A., Vijgen, P., and Woszidlo, R., "Low-Speed Performance Enhancement using Localized Active Flow Control - Localized Active Flow Control Simulations on a Reference Aircraft", NASA Technical Reports Server, April, 2022, document ID: 20220006731.
- 3. Vijgen, P., Ziebart, A., Shmilovich, A., and Woszidlo, R., "Low-Speed Performance Enhancement using Localized Active Flow Control - Integration Study of Localized Active Flow Control on a Performance Reference Aircraft", NASA Technical Reports Server, April, 2022, document ID: 20220006733.
- 4. Shmilovich, A., Stauffer, M., Woszidlo, R., and Vijgen, P., "Low-Speed Performance Enhancement using Localized Active Flow Control – Simulations, Scaling and Design of Localized Active Flow Control on the **Common Research** Model", NASA Technical Reports Server, April, 2022, document ID: 20220006736.

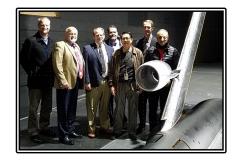
AIAA papers

- Shmilovich, A., Yadlin, Y., Vijgen, P., & Woszidlo, R., "Flow Control for Enhanced Aileron Effectiveness on a Commercial Aircraft," AIAA Paper 2023-0655, SciTech2023, 10.2514/6.2023-0655.
- 2. Shmilovich, A., Yadlin, Y., Vijgen, P., & Woszidlo, R., "Applications of Flow Control to Wing High-Lift Leading Edge Devices on a Commercial Aircraft," AIAA Paper 2023-0656, SciTech2023, 10.2514/6.2023-0656.
- Vijgen, P., Ziebart, A., Shmilovich, A., and Woszidlo, R., "Conceptual Integration Studies of Localized Active Flow Control on the Wing of a Commercial Aircraft," AIAA Paper 2023-0657, SciTech2023, 10.2514/6.2023-0657).

NASA Wind-Tunnel Model of the AFC-Enhanced Aileron

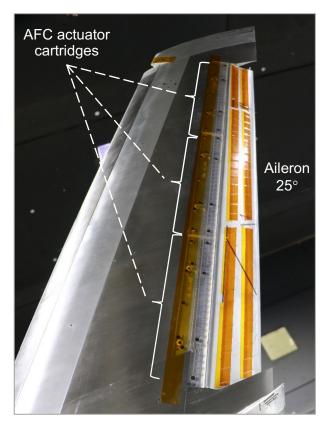
NASA Langley 14x22

- CRM-HL aileron AFC test
- 10% scale model
- Test conducted Feb-March, 2023











Courtesy of NASA

